

**DISPENSER ASSEMBLY FOR AEROSOLS HAVING  
LOW VOLATILE ORGANIC COMPOUND (VOC) CONTENT**

**[0001]** This application is a continuation-in-part of copending U.S. Patent Application No.10/350,011, entitled Aerosol Dispenser Assembly and Method of Reducing the Particle Size of a Dispensed Product, which was filed on January 24, 2003.

**FIELD OF THE INVENTION**

**[0002]** Our invention relates generally to the field of aerosol dispenser assemblies. More specifically, our invention relates to the field of aerosol dispenser assemblies using a liquefied gas propellant to expel a liquid product from a container.

**BACKGROUND OF THE INVENTION**

**[0003]** Aerosol dispensers have been commonly used to dispense personal, household, industrial, and medical products, and provide a low cost, easy to use method of dispensing such products. Typically, aerosol dispensers include a container, which contains a liquid product to be dispensed, such as soap, insecticide, paint, deodorant, disinfectant, air freshener, or the like. A propellant is used to discharge the liquid product from the container. The propellant is pressurized and provides a force to expel the liquid product from the container when a user actuates the aerosol dispenser by, for example, pressing an actuator button.

**[0004]** The two main types of propellants used in aerosol dispensers today are liquefied gas propellants, such as hydrocarbon and hydrofluorocarbon (HFC) propellants, and

J-3636A

compressed gas propellants, such as compressed carbon dioxide or nitrogen gas. To a lesser extent, chlorofluorocarbon propellants (CFCs) are also used. The use of CFCs is, however, being phased out due to the potentially harmful effects of CFCs on the environment.

[0005] In an aerosol dispenser using the liquefied gas-type propellant, the container is loaded with the liquid product and propellant to a pressure approximately equal to, or slightly greater than, the vapor pressure of the propellant. Thus filled, the container still has a certain amount of space that is not occupied by liquid. This space is referred to as the “head space” of the dispenser assembly. Since the container is pressurized to approximately the vapor pressure of the propellant, some of the propellant is dissolved or emulsified in the liquid product. The remainder of the propellant is in the vapor phase and fills the head space. As the product is dispensed, the pressure in the container remains approximately constant as liquid propellant evaporates to replenish discharged vapor. In contrast, compressed gas propellants are present entirely in the vapor phase. That is, no portion of a compressed gas propellant is in the liquid phase. As a result, the pressure within a compressed gas aerosol dispenser assembly decreases as the vapor is dispensed.

[0006] A conventional aerosol dispenser is illustrated in FIG. 3, and generally comprises a container (not shown) for holding a liquid product and a propellant, and a valve assembly for selectively dispensing a liquid product from the container. As illustrated in FIG. 3, the valve assembly comprises a mounting cup 106, a mounting gasket 108, a valve body 110, a valve stem 112, a stem gasket 114, an actuator cap 116, and a return spring 118. The valve stem 112, stem gasket 114, and return spring 118 are disposed within the valve body 110 and are movable relative to the valve body 110 to selectively control dispensing of the liquid product. The valve body 110 is affixed to the underside of the mounting cup 106, such that

J-3636A

the valve stem 112 extends through, and projects outwardly from, the mounting cup 106. The actuator cap 116 is fitted onto the outwardly projecting portion of the valve stem 112 and is provided with an exit orifice 132. The exit orifice 132 directs the spray of the liquid product into the desired spray pattern. A dip tube 120 is attached to the lower portion of the valve body 110 to supply the liquid product to the valve assembly to be dispensed. In use, the whole valve assembly is sealed to the container about its periphery by mounting gasket 108.

[0007] In operation, when the actuator cap 116 is depressed, the valve stem 112 is unseated from the mounting cup 106, which unseals the stem orifice 126 from the stem gasket 114 and allows the propellant to flow from the container, through the valve stem 112. Flow occurs because propellant forces the liquid product up the dip tube 120 and into the valve body 110 via a body orifice 122. In the valve body 110, the liquid product is mixed with additional propellant supplied to the valve body 110 through a vapor tap 124. The vapor tap 124 introduces additional propellant gas into the valve body 110, in order to help prevent flashing of the liquefied propellant, and to increase the amount of pressure drop across the exit orifice, which has the added benefit of further breaking-up the dispensed particles. From the valve body 110, the product is propelled through a stem orifice 126, out the valve stem 112, and through an exit orifice 132 formed in the actuator cap 116.

[0008] S.C. Johnson & Son, Inc. (S.C. Johnson) employs an aerosol valve similar to that shown in FIG. 3 in connection with their line of Glade® aerosol air fresheners. The propellant used to propel the air freshener liquid product from the container is a B-Series liquefied gas propellant having a propellant pressure of 40 psig (B-40), at 70 degrees F (2.72 atm at 294 K). "Propellant pressure" refers to the approximate vapor pressure of the propellant, as opposed to "can pressure," which refers to the initial gauge pressure contained

J-3636A

within a full aerosol container. The B-40 propellant is a composition of propane, normal butane, and isobutane. By normal butane it is meant the composition denoted by the chemical formula  $C_4H_{10}$ , having a linear backbone of carbon. This is in contrast to isobutane, which also has the chemical formula  $C_4H_{10}$ , but has a non-linear, branched structure of carbon. In order to effectively dispense this air freshener composition, the aerosol dispenser used by S.C. Johnson in connection with their line of Glade® aerosol air fresheners has a stem orifice diameter of 0.025" (0.635 mm), a vapor tap diameter of 0.020" (0.508 mm), a body orifice diameter of 0.062" (1.575 mm), and a dip tube inner diameter of 0.060" (1.524 mm). This current Glade® aerosol air freshener requires that the B-40 propellant be present in the amount of approximately 29.5% by weight of the contents of the dispenser assembly in order to satisfactorily dispense the air freshener liquid product.

[0009] Hydrocarbon propellants, such as B-40, contain Volatile Organic Compounds (VOCs). The content of VOCs in aerosol air fresheners is regulated by various federal and state regulatory agencies, such as the Environmental Protection Agency (EPA) and California Air Resource Board (CARB). S.C. Johnson continuously strives to provide environmentally friendly products and regularly produces products that exceed government regulatory standards. It is in this context that S.C. Johnson set out to produce an aerosol dispenser assembly having a reduced VOC content.

[0010] One way to reduce the VOC content in such aerosols is to reduce the amount of the propellant used to dispense the liquid product. However, we have discovered that a reduction in the propellant content adversely affects the product performance. Specifically, reducing the propellant content in the aerosol air freshener resulted in excessive product remaining in the container after the propellant is depleted (product retention), an increase in

J-3636A

the size of particles of the dispensed product (increased particle size), and a reduction in spray rate, particularly as the container nears depletion. It is desirable to minimize the particle size of a dispensed product in order to maximize the dispersion of the particles in the air and to prevent the particles from “raining” or “falling out” of the air. Thus, we set out to develop an aerosol dispenser assembly that can satisfactorily dispense an aerosol product that contains, at most, 25% by weight, of a liquefied gas propellant, while actually improving product performance throughout the life of the dispenser assembly.

[0011] The “life of the dispenser assembly” is defined in terms of the amount of propellant within the container (i.e., the can pressure), such that the life of the dispenser assembly is the period between when the pressure in the container is at its maximum (100% fill weight) and when the pressure within the container is substantially depleted, i.e., equal to atmospheric pressure. It should be noted that some amount of liquid product may remain at the end of the life of the dispenser assembly. As used herein, all references to pressure are taken at 70 °F (294 K), unless otherwise noted.

[0012] One known method of reducing the particle size of a dispensed liquid product is disclosed in U.S. Patent No. 3,583,642 to Crowell et al. (the '642 patent), which is incorporated herein by reference. The '642 patent discloses a spray head that incorporates a “breakup bar” for inducing turbulence in a product/propellant mixture prior to the mixture being discharged from the spray head. Such turbulence contributes to reducing the size of the mixture particles discharged from the spray head.

## SUMMARY OF THE INVENTION

[0013] Our invention provides an improved aerosol dispenser assembly that dispenses substantially all of a liquid product (i.e., reduces product retention) as a spray having a satisfactory particle size and spray rate, while at the same time reducing the amount of propellant required to dispense the liquid product from the container.

[0014] In one aspect, an aerosol dispenser assembly according to our invention comprises a container holding a liquid product and a liquefied gas propellant for propelling the liquid product from the container. The propellant is present in a quantity of at most about 25% by weight of the contents of the container. A valve is attached to the container for selectively dispensing the liquid product from the container as a mist. The assembly has a Clark/Valpey (CV) value of at most 25, where  $CV = 2.5(D-32) + 10|Q-1.1| + 2.6R$ , D being the average diameter in micrometers of particles dispensed during the first forty seconds of spray of the assembly, Q being the average spray rate in grams/second during the first forty seconds of spray of the assembly, and R being the amount of the product remaining in the container at the end of the life of the assembly expressed as a percentage of the initial fill weight. Preferably, the propellant is present in a quantity of between about 10% and about 25% by weight of the contents of the container.

[0015] In another aspect, an aerosol dispenser assembly according to our invention comprises a container holding a liquid product and a liquefied gas propellant for propelling the liquid product from the container. The propellant is present in a quantity of at most about 25% by weight of the contents of the container. A valve is attached to the container for selectively dispensing the liquid product and the propellant from the container. The valve

J-3636A

comprises a valve body and a valve stem. The valve body includes (i) a body orifice having a diameter of between about 1.270 and about 1.575 millimeters, for flow of the liquid product and propellant during dispensing, and (ii) a vapor tap having a diameter of between about 0.254 and about 0.483 millimeters, for introducing additional propellant gas through the valve body. The valve stem is disposed in the valve and defines at least one stem orifice having a total area of at least about 0.203 square millimeters, for flow of the liquid product and propellant during dispensing. A dispenser cap is coupled to the valve stem for actuating the valve to dispense the liquid product. The dispenser cap also defines an exit orifice having a diameter of between about 0.330 and about 0.635 millimeters, through which the liquid product and the propellant are dispensed.

[0016] In yet another aspect, an aerosol dispenser assembly according to our invention comprises a container holding a liquid product and a liquefied gas propellant for propelling the liquid product from the container. The propellant is present in a quantity of at most about 25% by weight of the contents of the container. A valve is attached to the container for selectively dispensing the liquid product and the propellant from the container. The valve comprises a valve body and a valve stem. The valve body includes (i) a body orifice having a diameter of between about 0.254 and about 0.635 millimeters, for flow of the liquid product and propellant during dispensing, and (ii) a vapor tap having a diameter of between about 0.076 and about 0.254 millimeters, for introducing additional propellant gas through the valve body. The valve stem is disposed in the valve and defines at least one stem orifice having a total area of at least about 0.405 square millimeters, for flow of the liquid product and propellant during dispensing. A dispenser cap is coupled to the valve stem for actuating the valve to dispense the liquid product. The dispenser cap also defines an exit orifice having

J-3636A

a diameter of between about 0.330 and about 0.635 millimeters, through which the liquid product and the propellant are dispensed.

[0017] In still another aspect, an aerosol dispenser assembly according to our invention comprises a container holding a liquid product and a liquefied gas propellant for propelling the liquid product from the container. The propellant is present in a quantity of at most about 15% by weight of the contents of the container. A valve is attached to the container and is capable of selectively dispensing the liquid product and the propellant from the container as a mist having a particle size in the range of about 15 micrometers to about 60 micrometers at a rate of between about 0.6 and about 1.8 grams/second, at least during the first forty seconds of spraying time of the life of the assembly.

[0018] Average particle size, as used herein, means average mean particle size  $D(V,0.5)$  of the dispensed product, as measured by laser diffraction analysis by a Malvern® Mastersizer 2600 Particle Size Analyzer, the aerosol assemblies being sprayed from a horizontal distance of 11-16.0" (27.5-40.6 cm) from the measurement area, and having a maximum cutoff size of 300 microns. This term is equivalent to mass mean particle size.

[0019] As used herein to describe any quantity, dimension, range, value, or the like, the term "about" is intended to encompass the range of error that occurs during any measurement, variations resulting from the manufacturing process, variation due to deformation during or after assembly, or variation that is the compounded result of one or more of the foregoing factors.



J-3636A

[0020] A better understanding of these and other aspects, features, and advantages of the invention may be had by reference to the drawings and to the accompanying description, in which preferred embodiments of the invention are illustrated and described.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0021] FIG. 1 is a cross-sectional perspective view of a first embodiment of the valve of the present invention.

[0022] FIG. 2 is a front view of the aerosol dispenser assembly of the first embodiment, with the container cut away for clarity.

[0023] FIG. 3 is an exploded view of a conventional aerosol valve assembly and actuator cap, illustrating the individual components.

[0024] Throughout the figures, like or corresponding reference numerals denote like or corresponding parts.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0025] As shown in FIG. 2, an aerosol dispenser assembly according to our invention generally comprises a container 2 with a valve assembly 4 disposed in the top thereof for selectively dispensing a liquid product from the container 2.

J-3636A

[0026] With reference to FIG. 1, the valve assembly 4 further comprises a mounting cup 6, a mounting gasket 8, a valve body 10, a valve stem 12, a stem gasket 14, an actuator cap 16, and a return spring 18. The actuator cap 16 defines an exit path 28 and an actuator orifice 32. The valve stem 12, stem gasket 14, and return spring 18 are disposed within the valve body 10 and are movable relative to the valve body 10. The valve body 10 is affixed to the underside of the mounting cup 6, such that the valve stem 12 extends through, and projects outwardly from, the mounting cup 6. The actuator cap 16 is fitted onto the outwardly projecting portion of the valve stem 12, and a dip tube 20 is attached to the lower portion of the valve body 10. The whole valve assembly 4 is sealed to the container 2 by mounting gasket 8.

[0027] While the dispenser assembly shown in FIG. 1 employs a vertical action-type cap 16, it will be understood that any suitable valve type may be used, such as, for example, a tilt action-type cap. In addition, instead of the simple push-button actuator cap 16 shown in FIG. 1, it will be understood that any suitable actuator may be used, such as, for example, an actuator button with an integral overcap, a trigger actuated assembly, or the like.

[0028] In operation, when the actuator cap 16 of the dispenser 1 is depressed, it forces the valve stem 12 to move downward, thereby allowing the liquid product to be dispensed. The propellant forces the liquid product up the dip tube 20 and into the valve body 10 via body orifice 22. In the valve body 10, the liquid product is mixed with additional propellant supplied to the valve body 10 through a vapor tap 24. The additional propellant introduced through the vapor tap 24 prevents flashing of the liquefied propellant, and increases the amount of pressure drop across the exit orifice which simultaneously increase the particle break-up. From the valve body 10, the liquid product is propelled through at least one stem

J-3636A

orifice 26, out the valve stem 12, and through an exit path 28 formed in the actuator cap 16.

A single stem orifice may be used; however, we have found that using two (as shown in FIG. 1), or preferably four, stem orifices 26 spaced around the periphery of the valve body 10 facilitates greater flow and superior mixing of the product as it is dispensed.

[0029] FIG. 1 depicts a breakup bar 30 in the exit path 28, such that the product is forced to diverge around the breakup bar 30, thereby inducing turbulence in the flow of the product, further reducing the particle size of the product. The product is then expelled from the actuator cap 16 through an actuator orifice 32, which disperses the product and produces a desired spray pattern. Instead of a breakup bar as shown in FIG. 1, the dispenser assembly might employ a pair of breakup plates positioned in or below the exit path 28, a swirl chamber positioned immediately upstream of the exit orifice 32, or other similar mechanical breakup features. While mechanical breakup features provide some additional break-up of the product prior to being dispensed, we have found that other factors have a much greater impact on particle size than these mechanical breakup features. Nonetheless, these mechanical breakup features may be used to even further reduce the size of the dispensed particles, but such mechanical breakup features are not necessary or preferred.

[0030] As noted above, we found that reducing the hydrocarbon propellant content of an aerosol air freshener to at most 25% by weight adversely affected the product performance. Specifically, reducing the propellant content in the aerosol air freshener resulted in excessive product retention, decreased spray rate as the container became depleted, and an increased particle size. Consequently, the air freshener exhibited excessive raining or falling out of the liquid product. In order to correct these adverse effects, we tested various different types of propellants, pressures, and valve orifice dimensions.

[0031] In particular, we tested two types of propellants, A-Series and B-Series propellants. Both types of propellants were found to be suitable for dispensing a liquid product from a container. We found, however, that the A-Series propellants that we tested unexpectedly produced a mist having a significantly smaller particle size than did the B-series propellants, under the same conditions. This difference was especially pronounced toward the end of the life of the dispenser assembly, when the pressure remaining in the container was lower. We believe that the superior mist producing ability of the A-Series propellants is due to the absence of normal butane in the A-Series propellants. As described above, the B-Series propellants contain a combination of propane, normal butane, and isobutane. In contrast, the A-series propellant does not contain any normal butane. When the dispenser assembly is shaken prior to use, the liquid product and the propellant form an oil-out emulsion. That is, small droplets of the liquid product are coated with a layer of fragrance oil and propellant, the aqueous phase liquid product being suspended in a layer of non-aqueous phase propellant and fragrance oil. When the emulsion is expelled from the pressurized dispenser assembly, the liquefied gas instantly evaporates, causing the droplets to “burst” and creating a fine mist of liquid product in the air. The absence of normal butane in the A-Series propellant is thought to facilitate a greater burst of mist, thereby reducing the particle size of the dispensed mist. This reduced particle size allows a greater amount of the dispensed product to remain suspended in the air for a longer period of time, thus, increasing the air freshening efficacy of the product.

[0032] While the invention is disclosed as being primarily used in connection with a hydrocarbon propellant, it should be understood that the invention could be adapted for use with other sorts of propellants. For example, HFC, dimethyl ether (DME), and CFC

J-3636A

propellants might also be used in connection with a variation of the dispenser assembly of our invention.

[0033] In addition, we tested various different propellant pressures and found that, in general, higher-pressure propellants tended to dispense the product as a mist having smaller particle size than did lower-pressure propellants. In addition, the higher-pressure propellants somewhat reduced the amount of product retained in the container at the end of the life of the dispenser assembly. However, simply increasing the pressure in the prior art aerosol dispensers, without more, was found to be insufficient to expel a satisfactory amount of the liquid product from the container. Thus, we also examined the aerosol valve itself to determine how best to reduce the amount of product retention, while maintaining a satisfactorily small particle size of the dispensed product.

[0034] In order to minimize the amount of product retention of the dispenser assembly, we found that it was desirable to increase the amount of liquid product dispensed per unit of propellant. That is, by making the dispensed ratio of liquid product to propellant smaller (i.e., creating a leaner mixture), the same amount of propellant will be able to exhaust a greater amount of liquid product. Several valve components are known to affect the dispensed ratio of liquid product to propellant, the vapor tap, the stem orifice, the body orifice, the exit orifice, and the inner diameter of the dip tube.

[0035] In general, we found that decreasing the size of the vapor tap has the effect of creating a leaner mixture. However, reducing the size of the vapor tap also has the side effect of increasing the particle size of the dispensed product. Conversely, we found that decreasing

J-3636A

the size of the stem orifice, body orifice, exit orifice and/or dip tube inner diameter generally decreases the spray rate and the particle size.

[0036] Based on the foregoing experimentation and analysis, we discovered that certain combinations of propellant type, can pressure, and valve orifice dimensions, produced a dispenser assembly that contains at most 25% by weight of a hydrocarbon propellant and has superior product performance over the prior art dispenser assemblies.

[0037] We also found that A-Series propellants, which are free from normal butane, exhibit reduced particle size of the dispensed product.

[0038] A dispenser assembly having a can pressure of between 55 psig (3.74 atm) and 120 psig (8.17 atm) was found to help reduce product retention while also reducing the particle size of the dispensed product. As noted above, can pressure refers to the initial gauge pressure contained within the aerosol container. Still higher pressures could also be effectively used to dispense the liquid product from the container. As the pressure within the aerosol dispenser assembly is increased, however, the strength of the aerosol dispenser container (also referred to as an aerosol can) must also be increased. Federal regulations (DOT ratings) govern the strength of pressurized containers and specify that aerosol cans must meet a certain can rating for a given internal pressure. Specifically, aerosol cans having an internal pressure of 140 psig or less at 130 °F (9.53 atm at 327 K) are known as “regular” or “unrated,” since a higher DOT rating is not required. Aerosol cans having an internal pressure of 160 psig or less at 130 °F (10.9 atm at 344 K) have a DOT rating of 2P, and cans having an internal pressure of 180 psig or less at 130 °F (12.3 atm at 355 K) have a DOT rating of 2Q. The higher the specified can rating, the stronger the aerosol can must be.

J-3636A

Generally, a can having a higher rating will be more costly due to increased material and/or manufacturing costs. Thus, in order to minimize costs, it is preferable to use the lowest pressure possible while still maintaining satisfactory product performance. In this regard, we found that can pressures of between 55 psig (3.74 atm) and 80 psig (5.44 atm), again measured at 70 degrees F (294 K), were especially preferred because they require a lower can rating than would higher can pressures and are still capable of achieving the advantages of the present invention (i.e., reduced propellant content, reduced particle size, and minimal product retention).

[0039] We also found that the dispenser assembly of FIG. 1 was capable of satisfactorily dispensing an aerosol product that contains at most 25% by weight of a liquefied gas propellant, when the diameter of the vapor tap 24 is between about 0.013" (0.330 mm) and about 0.019" (0.483 mm), the diameter of the stem orifice 26 is between about 0.020" (0.508 mm) and about 0.030" (0.762 mm) when a single stem orifice is used (between about 0.014" (0.356 mm) and about 0.025" (0.635 mm) when a pair of stem orifices are used), the diameter of the body orifice is between about 0.050" (1.270 mm) and about 0.062" (1.575 mm), the diameter of the exit orifice 32 is between about 0.015" (0.381 mm) and about 0.022" (0.559 mm), and the inner diameter of the dip tube is between about 0.040" (1.016 mm) and about 0.060" (1.524 mm).

[0040] Thus, any of the above-described valve components, propellant types, propellant pressures, and valve orifice dimensions, may be used in combination to provide a dispenser assembly according to our invention.

J-3636A

[0041] In a first preferred embodiment of the invention, the aerosol dispenser assembly 1 uses an A-Series propellant having a propellant pressure of about 60 psig (4.1 atm) (i.e., A-60 propellant) to dispense the liquid product from the container 2. In this embodiment, the container is initially pressurized to a can pressure of about 70 psig (4.8 atm) to about 80 psig (5.4 atm). The diameter of the vapor tap 24 in this embodiment is about 0.016" (0.406 mm). Two stem orifices 26 are used, each having a diameter of about 0.024" (0.610 mm). The diameter of the body orifice is about 0.050" (1.270 mm), the diameter of the exit orifice 32 is about 0.020" (0.508 mm), and the inner diameter of the dip tube is about 0.060" (1.52 mm). Furthermore, a breakup bar 30 is positioned in the exit path 28 of the actuator 16 in order to further reduce the particle size of the dispensed product.

[0042] A second preferred embodiment of the dispenser assembly 1 employs a single stem orifice 26. In this embodiment, the dispenser assembly 1 also uses the A-60 propellant and a can pressure of about 70 psig (4.8 atm) to about 80 psig (5.4 atm) to dispense the liquid product from the container 2. The diameter of the vapor tap is about 0.016" (0.406 mm), the diameter of the single stem orifice is about 0.025" (0.635 mm), the diameter of the body orifice is about 0.062" (1.575 mm), and the inner diameter of the dip tube is about 0.060" (1.524 mm). This embodiment also employs a breakup bar, positioned in the exit path of the actuator to further reduce the particle size of the dispensed product. The following table T.1 describes the performance of the dispenser assemblies according to the first and second preferred embodiments, respectively.

Propellant Type	A-60	A-60
Propellant Level (wt. %)	24.5	24.5
Body Orifice Diameter (mm)	1.58	1.27
Vapor Tap Diameter (mm)	0.406	0.406
Stem Orifice Area (mm <sup>2</sup> )	0.317	0.584



Exit Orifice Diameter (mm)	0.508	0.508
Dip Tube Diameter (mm)	1.52	1.52
Mechanical Breakup	Yes	Yes
Spray Rate (g/s) 100% Full	1.23	1.27
75% Full	1.18	1.15
50% Full	1.15	1.12
25% Full	1.07	1.05
Particle Size ( $\mu\text{m}$ ) 100% Full	29	29
75% Full	30	30
50% Full	29	32
25% Full	32	34
Retention (wt. %)	1.26	1.76

**T. 1 - Performance of Embodiments One and Two**

[0043] These preferred embodiments of the dispenser assembly are capable of dispensing the liquid product contained within the container as a mist having an average particle size of less than 35 micrometers (0.0014”), over at least 75% of the life of the dispenser assembly. Because the dispensed mist has such a small particle size, the particles are more easily dispersed in the air and less fallout is experienced. This reduction in the amount of fallout increases the dispenser assembly’s air freshening efficacy and helps to prevent undesirable residue of the liquid product from settling on flat surfaces, such as, countertops, tables, or floors.

[0044] Moreover, both preferred embodiments of the dispenser assembly are capable of dispensing over 98% by weight of the liquid product from the container. It is important that substantially all of the product can be dispensed, to ensure that product label claims will be met. Also, by minimizing the amount of product retained in the container at the end of the life of the dispenser assembly, less liquid product is wasted. This is important from a consumer satisfaction standpoint, since consumers tend to be more satisfied with a dispenser assembly when substantially all of the liquid product can be dispensed.

[0045] With the foregoing preferred embodiments as a threshold, we began to take a more focused approach to reducing the propellant content of a dispenser assembly even further. Our goal at this stage was to produce an aerosol dispenser assembly that could effectively dispense its contents using as little propellant as possible, but not more than about 15% liquefied gas propellant by weight. At the outset, we note that as the propellant content was reduced below about 15%, the stability of the product propellant emulsion began to break down. That is, at lower propellant levels, the oil-out emulsion inverted to a water-out emulsion, thereby deteriorating the performance characteristics. In contrast to an oil-out emulsion, a water-out emulsion contains small droplets of a non-aqueous phase suspended in an aqueous phase. We found that this inversion can be prevented by adjusting the emulsifier. For example, lowering the liquefied gas propellant level from 25% to 10% inverted the emulsion. Addition of 0.03% by weight of trimethyl stearyl ammonium chloride prevented the inversion. Of course, various other stabilizers in various different amounts may also be effectively used to prevent the inversion of the emulsion.

[0046] We first identified several “performance characteristics” upon which to measure the performance of a given dispenser assembly configuration. The performance characteristics identified were (1) the average diameter  $D$  in micrometers of particles dispensed during the first forty seconds of spray of the assembly, (2) the average spray rate  $Q$  in grams/second during the first forty seconds of spray of the assembly, and (3) the amount of the product  $R$  remaining in the container at the end of the life of the assembly, expressed as a percentage of the initial fill weight. As used herein, the term “fill weight” refers to the weight of all of the contents of the container, including both the liquid product and the propellant.

[0047] Based on consumer testing and air freshening efficacy, the particle size,  $D$ , should preferably be in the range of about 15 and about 60 micrometers, more preferably between about 25 and about 40 micrometers, and most preferably between about 30 and about 35 micrometers. The spray rate is preferably between about 0.6 and about 1.8 g/s, more preferably between about 0.7 and about 1.4 g/s, and most preferably between about 1.0 and about 1.3 g/s. The amount of liquid product remaining in the can at the end of life of the dispenser assembly is preferably less than about 3% of the initial fill weight, more preferably less than about 2% of the initial fill weight, and most preferably less than about 1% of the initial fill weight.

[0048] Next, we determined all of the factors that were known, or thought, to affect one or more of these performance characteristics. These factors included propellant content, dip tube inner diameter, body orifice diameter, vapor tap diameter, stem orifice diameter, mechanical breakup elements, exit orifice diameter, and land length (essentially the axial length of the exit orifice). Initial experiments were conducted, varying each of these factors individually, to determine the magnitude of the effect each factor had on the performance characteristics. The control platforms used for the initial testing were the original Glade dispenser assembly and the above-described first and second preferred embodiments. One or more of these platforms was then modified to vary each of the above factors individually. The magnitude of the effect each factor had on the performance characteristics was determined using a  $2^k$  factorial experimental design. The results of these calculations are shown graphically in FIG. 4.

J-3636A

**[0049]** From this list we selected the five factors (“critical factors”) having the greatest effect (negative or positive) on the performance characteristics to perform further experimentation. The critical factors selected were dip tube inner diameter, vapor tap diameter, body orifice diameter, stem orifice diameter, and exit orifice diameter.

**[0050]** While we knew that the critical factors had a pronounced effect on the performance characteristics, we were unsure if they varied independently of one another. To determine interdependencies, it was necessary to generate a table showing performance characteristics for every combination of every value of the critical factors within a desired range.

**[0051]** If each of the critical factors was varied through ten different sizes, it would have required one hundred thousand different trials to complete the table referred to above. Rather than run all of those different experiments, we used a Response Surface Method to select a limited sample of experiments. Based on our limited sample of experiments, we were able to generate a complete table of performance characteristics for every possible variation of the critical factors, using the Response Surface Method to interpolate the missing data points. Fifty-seven experiments were conducted -- a Box-Behnken Design consisting of twenty-nine experiments, the results of which are set forth in table T.2 below, and a D-Optimal Design consisting of twenty eight experiments, the results of which are set forth in table T.3 below. Descriptions of these two methods can be found in statistic text books such as “Design and Analysis of Experiments” by Douglas C. Montgomery, published by John Wiley and Sons, New York, 1997.

Trial	Exit Orifice (mm)	Vapor Tap (mm)	Dip Tube ID (mm)	Body Orifice (mm)	Particle Size Full (μm)	Particle Size @ 200g Fill Weight (μm)	Spray Rate Full (g/s)	Spray Rate @ 200g Fill Weight (g/s)	Retention (Wt. %)	CV
1	0.635	0.330	3.099	0.635	40.0	47.9	1.408	1.360	1.62	27
2	0.330	0.127	1.524	0.635	40.0	38.4	0.716	0.588	2.70	31
3	0.635	0.127	1.524	0.635	44.7	47.7	1.451	1.349	0.00	35
4	0.457	0.330	1.524	0.635	34.7	36.7	0.877	0.676	10.23	36
5	0.457	0.508	1.016	0.635	21.7	89.4	0.555	0.947	22.59	38
6	0.457	0.330	1.524	0.635	34.6	37.4	0.847	0.599	17.34	54
7	0.457	0.330	1.524	0.635	33.8	38.6	0.860	0.599	19.34	57
8	0.457	0.330	1.016	0.330	26.9	62.9	0.618	0.487	23.59	53
9	0.457	0.127	1.524	0.330	33.8	41.2	0.716	0.639	1.78	13
10	0.457	0.508	3.099	0.635	29.1	40.7	0.666	0.390	33.55	84
11	0.330	0.330	3.099	0.635	35.2	33.6	0.567	0.422	17.22	58
12	0.457	0.127	3.099	0.635	47.8	48.1	1.282	1.187	0.00	41
13	0.330	0.330	1.016	0.635	27.5	55.1	0.431	0.418	33.40	82
14	0.457	0.330	1.524	0.635	34.9	38.2	0.826	0.641	6.60	27
15	0.457	0.127	1.016	0.635	41.3	41.3	1.018	0.868	0.15	24
16	0.330	0.330	1.524	1.270	34.7	27.3	0.565	0.317	30.08	90
17	0.330	0.330	1.524	0.330	23.1	46.2	0.353	0.413	33.59	72
18	0.330	0.508	1.524	0.635	22.7	44.3	0.357	0.492	35.37	76
19	0.457	0.127	1.524	1.270	50.0	48.2	1.357	1.200	0.00	48
20	0.457	0.330	3.099	0.330	26.8	64.9	0.618	0.538	23.71	54
21	0.457	0.330	1.524	0.635	35.1	38.5	0.904	0.751	13.05	44
22	0.635	0.508	1.524	0.635	30.8	51.5	0.975	0.748	31.04	79
23	0.457	0.330	3.099	1.270	46.1	43.8	1.186	0.982	0.00	36
24	0.635	0.330	1.524	1.270	42.0	49.1	1.354	1.043	0.83	30
25	0.457	0.508	1.524	0.330	27.3	61.0	0.620	0.479	26.33	61
26	0.457	0.330	1.016	1.270	29.1	50.5	0.723	0.390	32.74	82
27	0.635	0.330	1.524	0.330	34.4	45.5	0.731	0.398	39.11	111
28	0.635	0.330	1.016	0.635	36.6	52.2	1.043	0.719	19.65	63
29	0.457	0.508	1.524	1.270	27.2	56.8	0.671	0.790	28.73	67

**T. 2 - Experimental Data for Box-Behnken Design**

Trial	Propellant Content (Wt. %)	Vapor Tap (mm)	Exit Orifice (mm)	Particle Size Full (μm)	Spray Rate Full (g/s)	Retention (Wt. %)
1	14.5	0.508	0.330	20.0	0.323	22.15
2	13	0.635	0.508	22.3	0.489	21.15
3	19	0.635	0.635	27.4	0.972	18.63
4	13	0.406	0.330	26.7	0.404	30.46

5	19	0.127	0.330	39.8	0.760	0.00
6	17	0.635	0.457	18.6	0.528	21.18
7	13	0.330	0.635	43.9	1.182	10.82
8	17	0.457	0.406	26.9	0.593	20.18
9	19	0.330	0.330	29.4	0.503	13.15
10	19	0.635	0.457	20.1	0.511	16.72
11	13	0.127	0.330	42.0	0.764	0.00
12	15	0.127	0.635	45.8	1.542	0.00
13	19	0.127	0.457	42.6	1.079	0.09
14	19	0.457	0.508	28.0	0.788	16.62
15	17	0.127	0.457	44.7	1.149	0.00
16	14.5	0.254	0.330	40.7	0.727	9.04
17	19	0.127	0.635	42.0	1.514	0.00
18	17.5	0.508	0.584	28.4	0.942	11.54
19	13	0.635	0.635	34.0	0.958	27.13
20	13	0.406	0.330	26.1	0.407	28.98
21	13	0.635	0.635	31.4	0.733	31.06
22	16	0.406	0.635	33.6	1.152	10.11
23	16	0.406	0.508	30.5	0.843	18.36
24	17	0.635	0.508	23.2	0.629	16.90
25	15	0.635	0.635	26.7	0.810	27.08
26	17	0.127	0.406	43.1	1.012	0.00
27	13	0.127	0.330	42.4	0.775	2.36
28	19	0.635	0.508	19.6	0.560	21.04

**T. 3 - Experimental Data for D-Optimal Design**

[0052] Each of the characteristics, D, Q, and R, was then weighted according to a number of different considerations, including its relative effect on the acceptability of the dispenser assembly to the consumer. The weighting process was iterated sequentially, through trial and error, until minimum values were achieved for samples known to have the best performance. The acceptability of the dispenser assembly to a consumer is given as the “quality” of the dispenser assembly and is represented by the Clark/Valpey (CV) factor -- smaller values of CV being more acceptable to consumers than larger ones. We found that, generally, a dispenser assembly having a quality value much greater than about 25 is unacceptable to most consumers. Accordingly, a dispenser assembly according to our invention should have a CV value of at most about 20, where  $CV = 2.5(D-32) + 10|Q-1.1| + 2.6R$ .

[0053] At a propellant level of 14.5% by weight and using an actuator cap 16 with a swirl chamber, we found that the body orifice diameter should preferably be between about 0.010" (0.254 mm) and about 0.025" (0.635 mm), and more preferably between about 0.010" (0.254 mm) and about 0.015" (0.381 mm). The vapor tap diameter should preferably be between about 0.003" (0.076 mm) and about 0.010" (0.254 mm), and more preferably between about 0.005" (0.127 mm) and about 0.008" (0.203 mm). The at least one stem orifice should preferably have a total area of at least about 0.000628 in<sup>2</sup> (0.405 mm<sup>2</sup>), and more preferably at least about 0.000905 in<sup>2</sup> (0.584 mm<sup>2</sup>). The exit orifice diameter should preferably be between about 0.013" (0.330 mm) and about 0.025" (0.635 mm), and more preferably between about 0.015" (0.381 mm) and about 0.022" (0.559 mm). And the dip tube inner diameter should preferably be between about 0.040" (1.016 mm) and about 0.122" (3.099 mm), and more preferably between about 0.050" (1.270 mm) and about 0.090" (2.286 mm). Not every combination of the above valve orifice dimensions will result in an aerosol dispenser assembly having a quality value of at most 25. However, most aerosol valves of this type having a quality value of at most 25 will have orifice dimensions that fall within the above ranges. Because the performance characteristics are not directly proportional to any one of the critical factors, and because the critical factors are not independent of one another, it is difficult to determine what combination of valve dimensions will result in the optimum quality of the dispensed spray. The tables T.4-T.8 below show how quality changes as the critical factors are varied through a representative range of values around the preferred valve configuration.

Vapor Tap (mm)	Body Orifice (mm)	Stem Orifice (mm <sup>2</sup> )	Dip tube (mm)	Exit Orifice (mm)	D (μm)	Q (g/s)	R (wt. %)	CV
0.127	0.330	1.824	1.524	0.457	36	0.72	0.58	15
0.127	0.457	1.824	1.524	0.457	46	1.08	0.46	36
0.127	0.635	1.824	1.524	0.457	48	1.17	0.54	42

**T.4 - Variation of Body Orifice Diameter**

Vapor Tap (mm)	Body Orifice (mm)	Stem Orifice (mm <sup>2</sup> )	Dip tube (mm)	Exit Orifice (mm)	D (μm)	Q (g/s)	R (wt. %)	CV
0.127	0.330	1.824	1.524	0.457	36	0.72	0.58	15
0.203	0.330	1.824	1.524	0.457	32	0.69	11.6	34
0.254	0.330	1.824	1.524	0.457	31	0.68	14.7	40

**T.5 - Variation of Vapor Tap Diameter**

Vapor Tap (mm)	Body Orifice (mm)	Stem Orifice (mm <sup>2</sup> )	Dip tube (mm)	Exit Orifice (mm)	D (μm)	Q (g/s)	R (wt. %)	CV
0.127	0.330	1.824	1.524	0.330	31	0.43	10.8	32
0.127	0.330	1.824	1.524	0.381	33	0.63	5.8	22
0.127	0.330	1.824	1.524	0.457	36	0.72	0.58	15
0.127	0.330	1.824	1.524	0.559	35	0.83	5.9	26
0.127	0.330	1.824	1.524	0.635	38	1.01	17.4	61

**T.6 - Variation of Exit Orifice Diameter**

Vapor Tap (mm)	Body Orifice (mm)	Stem Orifice (mm <sup>2</sup> )	Dip tube (mm)	Exit Orifice (mm)	D (μm)	Q (g/s)	R (wt. %)	CV
0.127	0.330	0.405	1.524	0.457	<36	<0.72	>0.58	<25
0.127	0.330	0.584	1.524	0.457	<36	<0.72	>0.58	<25
0.127	0.330	1.824	1.524	0.457	36	0.72	0.58	15

**T.7 - Variation of Stem Orifice Area**

Vapor Tap (mm)	Body Orifice (mm)	Stem Orifice (mm <sup>2</sup> )	Dip tube (mm)	Exit Orifice (mm)	D (μm)	Q (g/s)	R (wt. %)	CV
0.127	0.330	1.824	1.016	0.457	34	0.71	6.9	27
0.127	0.330	1.824	1.270	0.457	34	0.72	5.8	24
0.127	0.330	1.824	1.524	0.457	36	0.72	0.58	15
0.127	0.330	1.824	2.286	0.457	35	0.76	4.2	22
0.127	0.330	1.824	3.099	0.457	35	0.86	11.6	40

**T.8 - Variation of Dip Tube Inner Diameter**



J-3636A

[0054] From our complete tabular data, we were able to determine which combinations of valve orifice dimensions minimized the value of CV and provided the best performance at a propellant content of 14.5%. In particular, we found that a valve according to a third embodiment, having a body orifice diameter of about 0.013" (0.330 mm), a vapor tap diameter of about 0.005" (0.127 mm), an exit orifice diameter of about 0.018" (0.457 mm), a dip tube inner diameter of about 0.060" (1.524 mm), and at least one stem orifice having a total area of at least about 0.002827" (1.824 mm) provided the best performance for an aerosol air freshener. The third embodiment is substantially the same as the first embodiment in many respects, the main differences being the lower possible propellant content and the different ranges of orifice sizes. In this embodiment, A-60 propellant was again used as the propellant, and a swirl chamber mechanical breakup element was employed. Of course, no such mechanical breakup element is required.

[0055] The above tables were generated based on experimental data using dispenser assemblies having a propellant content of 14.5%. Gradual increases in propellant content, of course, significantly improve the quality of the dispensed sprays. Thus, by increasing the propellant content slightly, a broader range of valve orifice dimensions become acceptable. That is, a broader range of valve orifice dimensions will achieve an acceptable quality value. For example, simply increasing the propellant content of the preferred embodiment by 2%, the quality value was cut almost in half, from 15.3 to 8.8. We envision that many applications may benefit from using an aerosol dispenser assembly having a propellant content of less than 25%, but greater than the 14.5% achieved by our invention.

[0056] We believe it would be possible to produce an aerosol dispenser assembly that requires even less than 14.5% propellant to dispense its contents by employing some of the

J-3636A

other factors that were thought to affect the performance characteristics. For example, by providing an even smaller vapor tap, by incorporating some form of mechanical breakup element, by experimenting with different propellant types, by employing different land lengths, and/or by using different materials for construction, we envision being able to achieve satisfactory performance with as little as about 10% propellant content.

[0057] Of course, different products, such as paint, deodorant, hair fixatives, and the like, will have different material properties and may, therefore, require different valve orifice sizes. In addition, different products may have different spray characteristics that are acceptable to consumers. Therefore, a different formula for quality may have to be developed for each different product, in order to determine the appropriate valve orifice sizes for that product. We believe, however, that some products, such as insecticides, will have similar physical properties to the aerosol air fresheners upon which our study was based. Accordingly, we would expect such insecticides to have the same or similar formula for quality.

[0058] The embodiments discussed above are representative of preferred embodiments of the present invention and are provided for illustrative purposes only. They are not intended to limit the scope of the invention. Although specific components, configurations, materials, etc., have been shown and described, such are not limiting. For example, various other combinations of valve components, propellant types, propellant pressures, and valve orifice dimensions, can be used without departing from the spirit and scope of our invention, as defined in the claims. In addition, the teachings of the various embodiments may be combined with one another, as appropriate, depending on the desired performance characteristics of the valve.